

Shape estimation of concave specular object from multiview polarization
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1 Shape estimation of concave specular object from multiview 2 polarization

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7 **Abstract.** This paper proposes a method to estimate the surface normal of concave objects. The target object of our
8 method has specular surface without diffuse reflection. We solve the problem by analyzing the polarization state of
9 the reflected light. The polarization analysis gives a constraint to the surface normal. However, polarization data from
10 a single view has an ambiguity, and cannot uniquely determine the surface normal. In order to solve this problem, the
11 target object should be observed from two or more views. However, the polarization of the light should be analyzed
12 at the same surface point through different views. It means that both the camera parameters and the surface shape
13 should be known. The camera parameters can be estimated a-priori using known corresponding points. However, it
14 is a contradiction that the shape should be known in order to estimate the shape. In order to get out of a tough spot,
15 we assume that the target object is almost planar. Under this assumption, the surface normal of the object is uniquely
16 determined. This paper shows that the surface normal of the non-planar part can be also estimated using the proposed
17 method.

18 **Keywords:** polarization, shape-from-X, surface normal, concavity, specular reflection, crack.

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20 1 Introduction

21 Factories in industrial field have a high demand to estimate the shape of crack since it is quite
22 important for quality control of the products. Although there are many methods which detect
23 cracks,¹ little method have been proposed for estimating the shape of cracks. Therefore, there is
24 a great demand for estimating the shape of concave objects of highly specular surfaces, since it
25 is a challenging task. This paper proposes a method which estimates the surface normal of black
26 specular object with concave shape, by analyzing the polarization state of the reflected light, where
27 the target object is observed from multiple views.

28 3D modeling techniques have been intensively investigated in the field of computer vision. The
29 techniques used can be categorized into two types, the geometric approach and the photometric
30 approach. Geometric approach uses the geometrical structure of the scene, such as time-of-flight

31 laser range sensor, multinocular stereo, or structured light projection. Photometric approach uses
32 the light reflected from the scene, such as photometric stereo or shape-from-polarization. Shape-
33 from-specularity has been extensively surveyed by Ihrke et al.²

34 A smooth surface normal can be obtained using a photometric approach. Polarization³⁻⁵ is
35 one of the photometric clue that can be used to obtain a smooth surface normal. Koshikawa and
36 Shirai⁶ used circular polarization to estimate the surface normal of a specular object. Guarnera
37 et al.⁷ extended their method to determine the surface normal uniquely, by changing the lighting
38 conditions in two configurations. Morel et al.⁸ also disambiguated it using multiple illumination;
39 however, they did not solve the ambiguity of the degree of polarization (DOP)³⁻⁵ because they did
40 not use circular polarization. Saito et al.⁹ proposed the basic theory for estimating the surface
41 normal of a transparent object using polarization. Barbour¹⁰ approximated the relation between
42 the surface normal and the DOP and developed a commercial sensor for shape-from-polarization.
43 Kobayashi et al.¹¹ estimated the surface normal of transparent thin objects using DOP. They also
44 estimated the thickness by analyzing the light interference. Miyazaki et al.¹² estimated the surface
45 normal of a transparent object by analyzing the polarization state of the thermal radiation from the
46 object. Miyazaki et al.¹³ attempted to estimate the surface normal of a diffuse object from a single
47 view. Miyazaki et al.¹⁴ used a geometrical invariant to match the corresponding points from two
48 views to estimate the surface normal of a transparent object. Miyazaki and Ikeuchi¹⁵ solved the
49 inverse problem of polarization ray tracing to estimate the surface normal of a transparent object.
50 These methods first calculate the polarization data from input images, while Yu et al.¹⁶ used the
51 input images themselves to estimate the surface normal without explicitly calculating the DOP.

52 Wolff and Boulton¹⁷ developed the basic theory for showing that polarization analysis can es-
53 timate a surface normal from two views if the corresponding points are known. Rahmann and

54 Canterakis¹⁸ estimated the surface normal of a specular object from multiple views by iteratively
55 finding the corresponding points of these views. Rahmann¹⁹ proved that only the quadratic sur-
56 faces are estimated if the corresponding points are searched iteratively. Atkinson and Hancock²⁰
57 analyzed the local structure of an object to find the corresponding points between two viewpoints
58 in order to calculate the surface normal from the polarization of two views. Atkinson and Han-
59 cock²¹ also provided a detailed investigation of surface normal estimation for a diffuse object from
60 a single view. Huynh et al.²² estimated not only the surface normal but also the refractive index.

61 Kadambi et al.²³ combined the 3D geometry obtained by a time-of-flight (ToF) sensor and
62 the surface normal obtained from the DOP. Smith et al.²⁴ combined the depth sensor and the
63 shape-from-polarization. Cui et al.²⁵ used structure-from-motion while Yang et al.²⁶ used SLAM
64 in addition to the shape-from-polarization. Miyazaki et al.²⁷ combined the visual hull and the
65 shape-from-polarization.

66 In this study, we propose a method for creating a 3D model using both polarization analysis
67 and planarity assumption. The principal target objects are smooth surfaces with high specular re-
68 flection and low diffuse reflection which are annoying targets in conventional techniques. We first
69 calibrate multiple cameras to calculate the geometrical relationships among them. We observe the
70 object from multiple viewpoints using a polarization imaging camera. In order to determine the
71 corresponding point among multiple views, we assume the target object as planar. However, this
72 assumption solely can simply produce a planar shape, thus we additionally use polarization infor-
73 mation in order to estimate the non-planar part of the object. The shape-from-polarization method
74 can estimate the shape of black objects with high specularity, which cannot be estimated using
75 the photometric stereo method because there are no diffuse reflections. The polarization informa-
76 tion of the object is obtained from multiple viewpoints using a polarization imaging camera. The

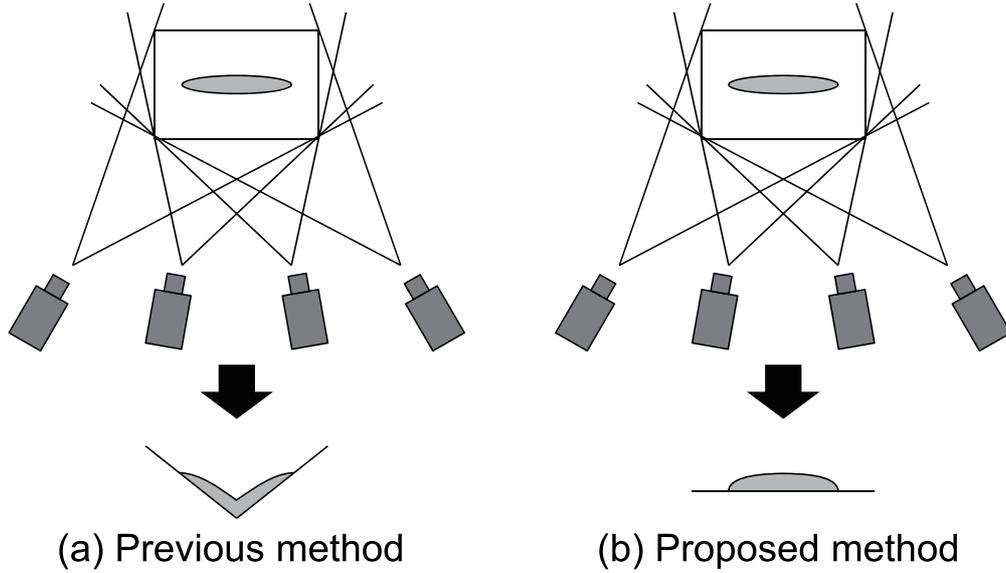


Fig 1 Our contribution: (a) Previous method which is based on visual hull which is not suited to estimate planar shapes and (b) proposed method which is suited to estimate concave shapes which is almost planar.

77 polarization data must be analyzed at identical points on the object surface when observed from
 78 multiple viewpoints; thus, the planarity assumption can be used for estimating the surface normal
 79 from polarization data. The target object of our method is almost planar except for a crack with
 80 small size.

81 Miyazaki’s method²⁷ relies on the visual hull. It is difficult to estimate a planar shape using
 82 visual hull, and in addition, it is impossible to estimate a planar shape with infinite size (Fig. 1
 83 (a)). Our method can also be applied to infinite plane (Fig. 1 (b)), thus, our method overcomes the
 84 disadvantage of their method,²⁷ which means that the proposed method is fundamentally superior
 85 than their method²⁷ if the target object is almost planar.

86 We describe our method in Section 2 and present our results in Section 3. The theory shown
 87 in Section 2 assumes that the target object must be completely planar. However, Section 3 empiri-
 88 cally proves that our method can successfully estimate the surface normal even if the object is not
 89 completely planar. We discuss the advantages and disadvantages of our method and conclude the

90 paper in Section 4.

91 **2 Using polarization in estimating the surface normal of concave objects**

92 *2.1 Algorithm flow*

93 First, we explain the flow of our method (Fig. 2).

94 Since we observe the target object from multiple viewpoints, we calibrate each viewpoint in
95 order to obtain each camera parameter. Although any calibration pattern works well, this paper
96 assumes that each camera is calibrated using four points marked at the vertices of square for clarity.
97 The area which is surrounded by these markers is the target area. Using these markers, we estimate
98 the homography \mathbf{H} (Section 2.6) and rotation \mathbf{R} (Section 2.5). Fig. 3 shows the homographic
99 projection from each view to canonical square. Canonical square can be any square defined by the
100 engineer.

101 Polarization camera captures the azimuth angle ϕ of the target object (Section 2.2). We denote
102 the 90° rotation of ϕ as vector \mathbf{a} , which would be orthogonal to surface normal (Section 2.3). Using
103 the vector \mathbf{a} and rotation matrix \mathbf{R} of camera parameter, surface normal \mathbf{n} is calculated using SVD
104 (singular value decomposition) (Section 2.4).

105 Finally, surface normal is integrated to height field.¹⁵

106 *2.2 Polarization*

107 We explain only linear polarization since circular polarization is not related to our method. Light is
108 an electromagnetic wave, and electromagnetic wave oscillating in only one direction is said to have
109 perfectly linear polarization, while electromagnetic wave oscillating isotropically in all directions
110 is called unpolarized light. The intermediate state of such light is called partially polarized light.

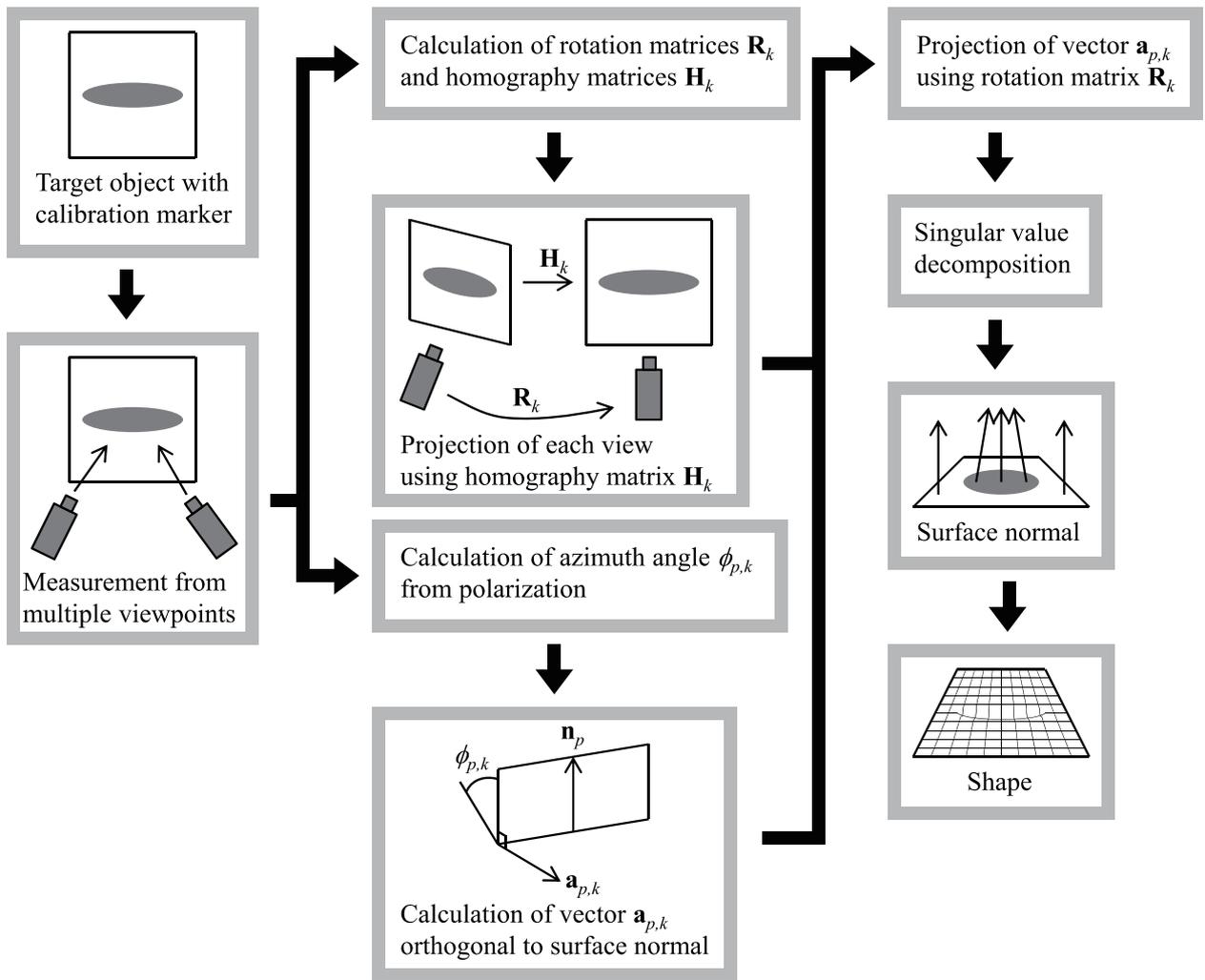


Fig 2 Algorithm flow.

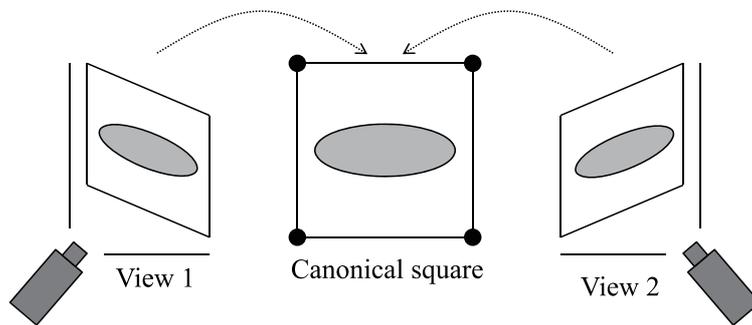


Fig 3 Transformation to canonical square.

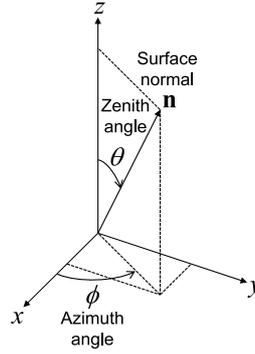


Fig 4 Polar coordinates of surface normal.

111 DOP (degree of polarization)³⁻⁵ is one of the metrics used to represent the polarization state of
 112 light. Its value varies from 0 to 1, with 1 representing perfectly polarized light and 0 representing
 113 unpolarized light.

114 The maximum light observed while rotating the polarizer is denoted as I_{\max} , and the minimum
 115 light is denoted as I_{\min} . In this paper, the polarizer angle at which I_{\min} is observed is called the
 116 azimuth angle ϕ . The surface normal is represented in polar coordinates, where the azimuth angle
 117 is denoted as ϕ and the zenith angle is denoted as θ (Fig.4). The azimuth angle calculated from
 118 the polarization has 180° -ambiguity since linear polarizer has 180° cycle. Thus, the azimuth angle
 119 of the surface normal will be either ϕ or $\phi + 180^\circ$. The plane consisting of the incident light and
 120 surface normal vectors is called the reflection plane. The reflected light vector is also coplanar
 121 with the reflection plane since the surface is optically smooth. The orientation of the reflection
 122 plane is the same as the azimuth angle ϕ and $\phi + 180^\circ$, which is defined on a certain xy -plane and
 123 is defined as an angle between x -axis and the reflection plane projected on xy -plane. Since we
 124 capture images with a camera, the x -axis and the y -axis of the image coordinates is used.

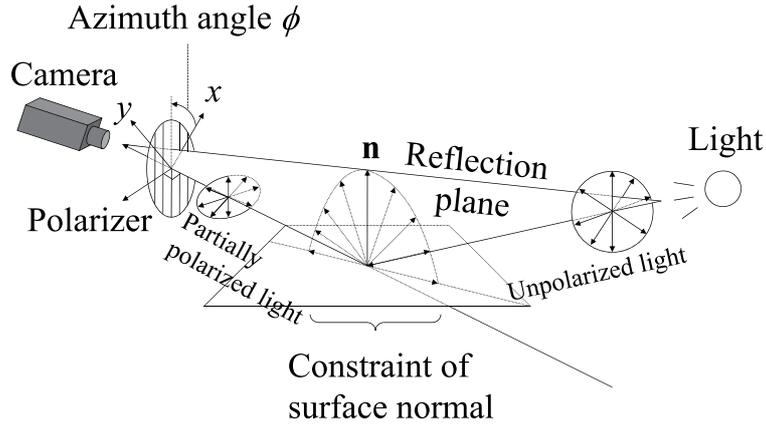


Fig 5 Relationship between the surface normal and the reflection plane when observed from a single viewpoint.

125 *2.3 Calculating the surface normal from two viewpoints*

126 Section 2.2 described the relationship between the surface normal and the azimuth angle obtained
 127 from polarization. However, we cannot determine the surface normal uniquely because only the
 128 orientation of the reflection plane including the surface normal is obtained. We must observe the
 129 object from two viewpoints to solve this problem.

130 Fig. 5 represents the situation of our problem. A camera has its coordinate system x -axis, y -
 131 axis, and z -axis. Camera's z -axis is along the optical axis. The reflection plane angle ϕ is the angle
 132 between the x -axis of camera coordinate system and the line caused by the intersection between
 133 the reflection plane and the xy -plane.

We analyze the two reflection plane angles at the same surface point, corresponding to the known 3D geometry. Our method assumes that the 3D geometry of the target object is almost a plane. The relationship between the surface normal vector and the azimuth angle is shown in Fig. 6. The relationship between the azimuth angles for each of the cameras, represented as ϕ_1 and

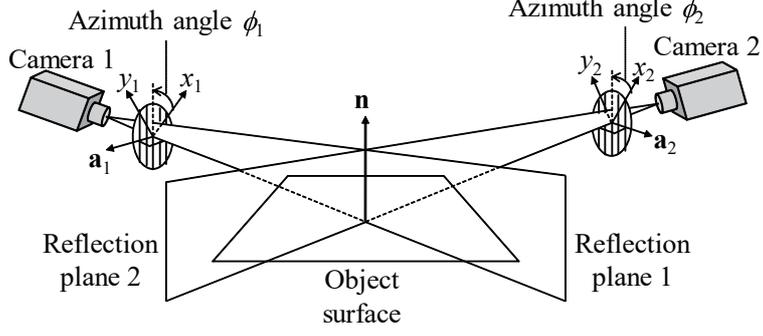


Fig 6 Relationship between the surface normal and the reflection plane when observed from two viewpoints.

ϕ_2 , and the normal vector of the reflection plane, represented as \mathbf{a}_1 and \mathbf{a}_2 , is shown in Eq. (1).

$$\mathbf{a}_1 = \begin{pmatrix} \cos(\phi_1 + 90^\circ) \\ \sin(\phi_1 + 90^\circ) \\ 0 \end{pmatrix}, \quad \mathbf{a}_2 = \begin{pmatrix} \cos(\phi_2 + 90^\circ) \\ \sin(\phi_2 + 90^\circ) \\ 0 \end{pmatrix}. \quad (1)$$

134 As shown in Fig. 6, the surface normal \mathbf{n} is orthogonal to the vectors \mathbf{a}_1 and \mathbf{a}_2 . After projecting
 135 the vectors \mathbf{a}_1 and \mathbf{a}_2 to the world coordinate system, we can calculate the surface normal \mathbf{n} .
 136 The rotation matrix projecting the world coordinate system to each camera coordinate system is
 137 represented as \mathbf{R}_1 and \mathbf{R}_2 . The inverse of each of these rotation matrices is its transpose, and
 138 they project back from the camera coordinate system to the world coordinate system. Thus, this
 139 situation is represented as Eq. (2).

$$\begin{pmatrix} \mathbf{a}_1^\top \mathbf{R}_1 \\ \mathbf{a}_2^\top \mathbf{R}_2 \\ \mathbf{0}^\top \end{pmatrix} \begin{pmatrix} n_x \\ n_y \\ n_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}. \quad (2)$$

140 Namely, the world coordinate of \mathbf{a}_1 and \mathbf{a}_2 are $\mathbf{R}_1^\top \mathbf{a}_1$ and $\mathbf{R}_2^\top \mathbf{a}_2$. Since $\mathbf{R}_1^\top \mathbf{a}_1$ and $\mathbf{R}_2^\top \mathbf{a}_2$ are
 141 orthogonal to the surface normal \mathbf{n} , $(\mathbf{R}_1^\top \mathbf{a}_1) \cdot \mathbf{n} = 0$ and $(\mathbf{R}_2^\top \mathbf{a}_2) \cdot \mathbf{n} = 0$ hold. These formulae can

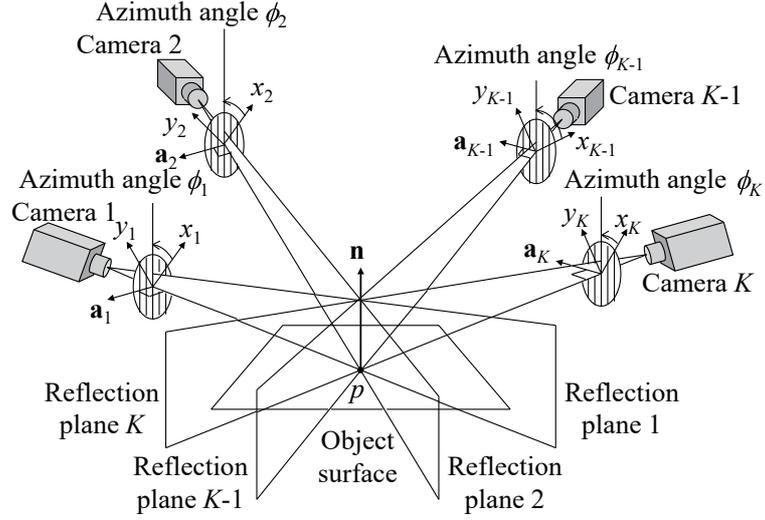


Fig 7 Relationship between the surface normal and the azimuth angle observed from multiple viewpoints.

142 be expressed, in other form, as $\mathbf{a}_1^\top \mathbf{R}_1 \mathbf{n} = 0$ and $\mathbf{a}_2^\top \mathbf{R}_2 \mathbf{n} = 0$ (Eq. (2)).

143 2.4 Calculating the surface normal from multiple viewpoints

144 This section explains the estimation process for the surface normal from the azimuth angle obtained
 145 from multiple viewpoints.

146 Fig. 7 shows the relationship between the surface normal \mathbf{n} of the surface point p and the
 147 azimuth angle obtained from K viewpoints. In Fig. 7, ϕ_k represents the azimuth angle of the
 148 surface point p observed by the camera $k = (1, 2, \dots, K)$, and \mathbf{a}_k represents the vector orthogonal
 149 to the reflection plane under the coordinate system of the camera k .

The rotation matrix \mathbf{R}_k represents the transformation from the world coordinate system to the

local coordinate system of the camera indicated by k . Similar to Eq. (2), Eq. (3) or Eq. (4) holds.

$$\begin{pmatrix} \mathbf{a}_1^\top \mathbf{R}_1 \\ \mathbf{a}_2^\top \mathbf{R}_2 \\ \vdots \\ \mathbf{a}_K^\top \mathbf{R}_K \end{pmatrix} \begin{pmatrix} n_x \\ n_y \\ n_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 0 \end{pmatrix}, \quad (3)$$

or in other form,

$$\mathbf{A}\mathbf{n} = \mathbf{0}. \quad (4)$$

The surface normal \mathbf{n} , which satisfies Eq. (4) in the least-squares sense, can be estimated using SVD (singular value decomposition).²⁸ The $K \times 3$ matrix \mathbf{A} can be decomposed by SVD as follows.

$$\begin{pmatrix} \mathbf{a}_1^\top \mathbf{R}_1 \\ \mathbf{a}_2^\top \mathbf{R}_2 \\ \vdots \\ \mathbf{a}_K^\top \mathbf{R}_K \end{pmatrix} = \mathbf{U}\mathbf{W}\mathbf{V}^\top = \mathbf{U} \begin{pmatrix} w_1 & & \\ & w_2 & \\ & & 0 \end{pmatrix} \begin{pmatrix} \mathbf{v}_1 \\ \mathbf{v}_2 \\ \mathbf{v}_3 \end{pmatrix}. \quad (5)$$

150 Here, \mathbf{U} is a $K \times 3$ orthogonal matrix, \mathbf{W} is a 3×3 diagonal matrix with non-negative values, and
 151 \mathbf{V}^\top is a 3×3 orthogonal matrix. The diagonal element w_i of the matrix \mathbf{W} is the singular value of
 152 the matrix \mathbf{A} and the singular vector corresponding to w_i is \mathbf{v}_i . Owing to the relationship between
 153 the surface normal and the reflection planes, the rank of the matrix \mathbf{A} is at most 2; thus, one of the
 154 three singular values becomes 0. Please see Miyazaki²⁷ for the proof. The surface normal \mathbf{n} can
 155 be represented as Eq. (6),²⁸ which can be calculated from the singular vector that has the smallest

156 singular value, namely, the third row of \mathbf{V}^\top in Eq. (5).

$$\mathbf{n} = s\mathbf{v}_3^\top. \quad (6)$$

157 In general, s is an arbitrary scalar coefficient; however, since the surface normal and the singular
 158 vectors are normalized vectors, s would be either $+1$ or -1 . Whether s be positive or negative is
 159 determined so that the surface normal faces toward the camera. The surface normal estimated by
 160 Eq. (6) is the optimal value that minimizes the squared error of Eq. (4) formulated by K equations.
 161 The input data must be obtained from two or more viewpoints since the rank of the matrix \mathbf{A} is 2.

162 2.5 Camera parameters

163 Eq. (3) or Eq. (4) calculates the surface normal from the azimuth angle under multiple viewpoints.
 164 In order to solve Eq. (4), the azimuth angle should be analyzed at corresponding points among
 165 multiple viewpoints. The corresponding points are determined by homography as shown in Section
 166 2.6. Eq. (4) also requires the rotation matrices of each camera. Namely, the extrinsic parameter of
 167 each camera should be known.

168 Our paper represents the projection from 3D vertex (X, Y, Z) to 2D vertex (x, y) as Eq. (7).²⁹

$$\begin{pmatrix} x \\ y \\ 1 \end{pmatrix} \sim \begin{pmatrix} f & 0 & 0 \\ 0 & f & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} r_{11} & r_{12} & r_{13} & t_1 \\ r_{21} & r_{22} & r_{23} & t_2 \\ r_{31} & r_{32} & r_{33} & t_3 \end{pmatrix} \begin{pmatrix} X \\ Y \\ Z \\ 1 \end{pmatrix}. \quad (7)$$

169 In Eq. (7), we skip to describe the camera center parameter (C_x, C_y) for clarity, since we assume

170 pinhole camera model. We skip to explain the detailed implementation to estimate these parameters

171 $f, t_1, t_2, t_3, r_{11}, r_{12}, \dots, r_{33}$.

172 2.6 Homography transform

173 Homography is a projection from a certain quadrangle to another certain quadrangle represented

174 under the homographic projection. Homography represents one-to-one correspondence between

175 two planes without redundancy nor lack of information. Therefore, it is natural to use homography

176 in our work since the target object is almost planar.

Homogeneous coordinate is defined as follows using (ξ_1, ξ_2, ξ_3) ($\xi_3 \neq 0$), where one element is added to the coordinates (x', y') .

$$x' = \frac{\xi_1}{\xi_3}, \quad y' = \frac{\xi_2}{\xi_3}. \quad (8)$$

177 Homographic projection from a certain quadrangle (x, y) to another certain quadrangle (x', y')

178 can be represented as follows.

$$\begin{pmatrix} x' \\ y' \\ 1 \end{pmatrix} \sim \begin{pmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{pmatrix} = \begin{pmatrix} h_{11} & h_{12} & h_{13} \\ h_{21} & h_{22} & h_{23} \\ h_{31} & h_{32} & h_{33} \end{pmatrix} \begin{pmatrix} x \\ y \\ 1 \end{pmatrix}. \quad (9)$$

179 Namely, homographic projection is represented by homography matrix $h_{11}, h_{12}, \dots, h_{33}$. Point

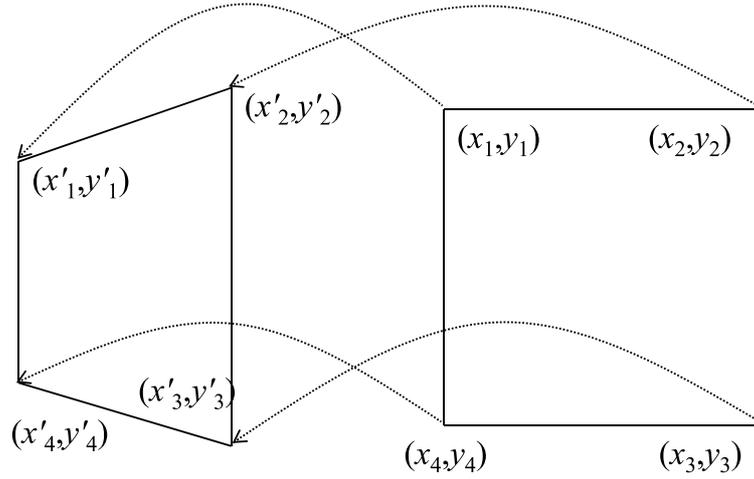


Fig 8 Homographic projection from a certain quadrangle to another certain quadrangle.

180 (x, y) is projected to the point $(x', y') = (\xi_1/\xi_3, \xi_2/\xi_3)$ by this homography matrix.

$$x' = \frac{h_{11}x + h_{12}y + h_{13}}{h_{31}x + h_{32}y + h_{33}}, \quad (10)$$

181

$$y' = \frac{h_{21}x + h_{22}y + h_{23}}{h_{31}x + h_{32}y + h_{33}}. \quad (11)$$

182 Fig. 8 is an example where vertices of quadrangle (x_1, y_1) , (x_2, y_2) , (x_3, y_3) , and (x_4, y_4) cor-
 183 respond to vertices of quadrangle (x'_1, y'_1) , (x'_2, y'_2) , (x'_3, y'_3) , and (x'_4, y'_4) .

184 Scaling the 3×3 homography matrix $h_{11}, h_{12}, \dots, h_{33}$ results in same transformation, thus, we
 185 fix one element as follows in order to uniquely determine the homography matrix.

$$h_{33} = 1. \quad (12)$$

186 Substituting the above equation into Eqs. (10)–(11) results in Eqs. (13)–(14).

$$xh_{11} + yh_{12} + h_{13} - xx'h_{31} - yy'h_{32} = x', \quad (13)$$

187

$$xh_{21} + yh_{22} + h_{23} - xy'h_{31} - yy'h_{32} = y'. \quad (14)$$

188 Concatenating Eqs. (13)–(14) for four vertices results in Eq. (15).

$$\begin{pmatrix} x_1 & y_1 & 1 & 0 & 0 & 0 & -x_1x'_1 & -y_1y'_1 \\ 0 & 0 & 0 & x_1 & y_1 & 1 & -x_1y'_1 & -y_1y'_1 \\ x_2 & y_2 & 1 & 0 & 0 & 0 & -x_2x'_2 & -y_2x'_2 \\ 0 & 0 & 0 & x_2 & y_2 & 1 & -x_2y'_2 & -y_2y'_2 \\ x_3 & y_3 & 1 & 0 & 0 & 0 & -x_3x'_3 & -y_3x'_3 \\ 0 & 0 & 0 & x_3 & y_3 & 1 & -x_3y'_3 & -y_3y'_3 \\ x_4 & y_4 & 1 & 0 & 0 & 0 & -x_4x'_4 & -y_4x'_4 \\ 0 & 0 & 0 & x_4 & y_4 & 1 & -x_4y'_4 & -y_4y'_4 \end{pmatrix} \begin{pmatrix} h_{11} \\ h_{12} \\ h_{13} \\ h_{21} \\ h_{22} \\ h_{23} \\ h_{31} \\ h_{32} \end{pmatrix} = \begin{pmatrix} x'_1 \\ y'_1 \\ x'_2 \\ y'_2 \\ x'_3 \\ y'_3 \\ x'_4 \\ y'_4 \end{pmatrix}. \quad (15)$$

189 Since we have 8 unknowns ($h_{11}, h_{12}, \dots, h_{32}$) and 8 equations (8 rows of the leftmost matrix in

Eq. (15)), closed-form solution exists. Solving this results in homography matrix shown below

$$\mathbf{H} = \begin{pmatrix} h_{11} & h_{12} & h_{13} \\ h_{21} & h_{22} & h_{23} \\ h_{31} & h_{32} & 1 \end{pmatrix}. \quad (16)$$

Using the homography matrix \mathbf{H} (Eq. (16)), the corresponding points between two quadrangles (Fig. 8) can be expressed by Eq. (9). Suppose that the homography of camera 1 is \mathbf{H}_1 and that of camera 2 is \mathbf{H}_2 . Fig. 3 shows the homographic projection from each view to canonical square. Canonical square can be any square defined by the engineer. Suppose that the pixel position of the canonical square is (x, y) . The corresponding points of camera 1 (x'_1, y'_1) and camera 2 (x'_2, y'_2) can be calculated as follows.

$$\begin{pmatrix} x'_1 \\ y'_1 \end{pmatrix} \sim \mathbf{H}_1 \begin{pmatrix} x \\ y \end{pmatrix}, \quad \begin{pmatrix} x'_2 \\ y'_2 \end{pmatrix} \sim \mathbf{H}_2 \begin{pmatrix} x \\ y \end{pmatrix}. \quad (17)$$

Namely, the two points (x'_1, y'_1) and (x'_2, y'_2) are corresponded while the point (x, y) acted as a mediator.

3 Experiment

3.1 Experimental setup

As is shown in Fig. 9, the target object is surrounded by white material. This white environment acts as a light source, and illuminates the target object from every direction. Cheap foaming polystyrene is used in our experiment, and it is located not strictly but roughly. Once we set this white enclosure, we do not need to move it like photometric stereo, which needs to move the light

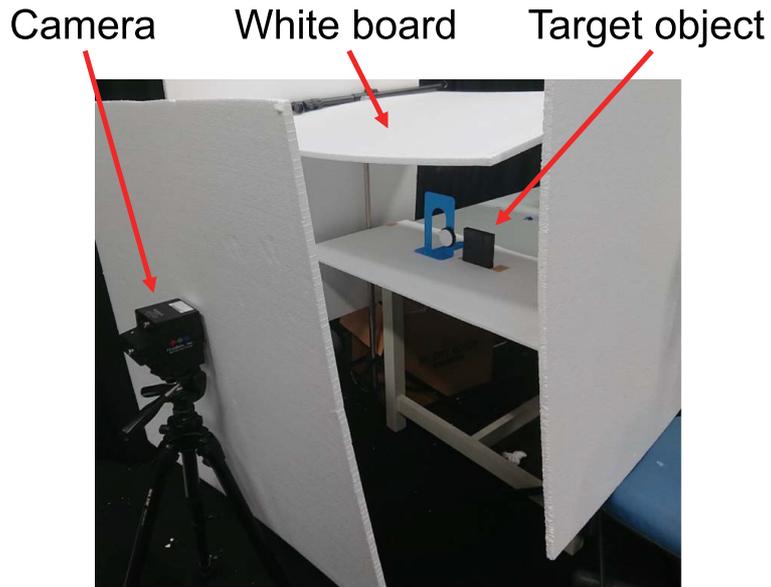


Fig 9 Experimental environment.

Table 1 Specification of the camera.

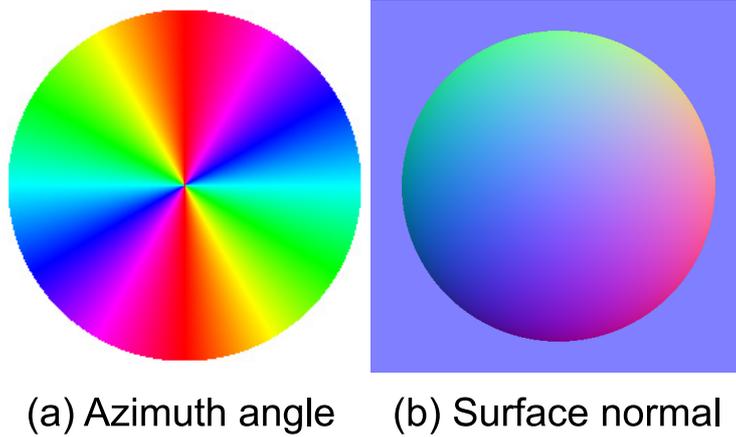
Manufacturer	FluxData Inc., NY
Product name	FD-1665P
Sensor	Sony ICX414
Resolution	659×494
Pixel size	$9.9\mu m \times 9.9\mu m$
Configuration	0, 45, 90 linear polarizer
Frame rate	74fps
Interface	IEEE-1394b

199 sources. The white board is illuminated by ordinary room light which is set in ordinary room.
 200 Often, the white board is unnecessary, since wall, floor, and ceil act as an illuminator.¹⁸

201 The camera we used is shown in Fig. 10 and Table 1. Since we have only one camera (because
 202 polarization camera is expensive), we rotated the target object instead of rotating the camera. Note
 203 that, observing a target object with multiple cameras and observing the target object rotated in
 204 multiple angles with a single camera are mathematically same.



Fig 10 Polarization camera.



(a) Azimuth angle (b) Surface normal

Fig 11 Pseudo color representation of an ideal sphere: (a) Azimuth angle and (b) surface normal.

205 *3.2 Pseudo color representation of the result*

206 Following sections show some results of our method. For visualization, the azimuth angle and the
207 surface normal are represented by pseudo-color. Fig. 11 (a) and Fig. 11 (b) show the pseudo color
208 representation of the azimuth angle and the surface normal of ideal hemishpere, respectively.

209 3.3 Result of ellipsoid

210 The target object is shown in Fig. 12. We generated the object using 3D printer, so that we can
211 compare the result with the ground truth, which is the digital data input to the 3D printer. The
212 size of the square is 10 [cm] \times 10 [cm], the diameter of long axis of the ellipse is 7.5 [cm], the
213 diameter of short axis of the ellipse is 2.5 [cm], and the maximum deepness of the concave part is
214 0.625 [cm]. The unique characteristic of our method is that we can estimate a shape of cracks. First
215 of all, we evaluate the performance of the proposed method. In order to guarantee the statistical
216 reliability, we need to estimate the surface normal with wide variety and wide area. That is why
217 we first measure the concave ellipsoid.

218 We took one image each from 15 different direction (Fig. 13). Pseudo-color representation of
219 surface normal of our method is shown in Fig. 14, and that of ground truth is shown in Fig. 15.
220 Note that our method successfully estimated the shape which is almost the same as true shape. The
221 estimated shape is shown in Fig. 16 and Fig. 18 (c), while ground truth is shown in Fig. 17 and
222 Fig. 18 (a). The error is calculated as the angle between two surface normals of the estimated and
223 the ground truth. Error is shown in Fig. 19 (b), where the average error was 4.49 [deg].

224 3.4 Comparison to photometric stereo

225 In order to prove the effectiveness of our method, we compare our method with the result of
226 photometric stereo.³⁰

227 Photometric stereo from 15 lights is applied to the object shown in Fig. 12, and the input
228 images are shown in Fig. 20. Surface normal of the photometric stereo is shown in Fig. 21, and
229 the estimated shape is shown in Fig. 22 and Fig. 18 (b). Photometric stereo assumes Lambertian
230 reflection though the actual reflection is specular reflection, thus, the shape is distorted. The error

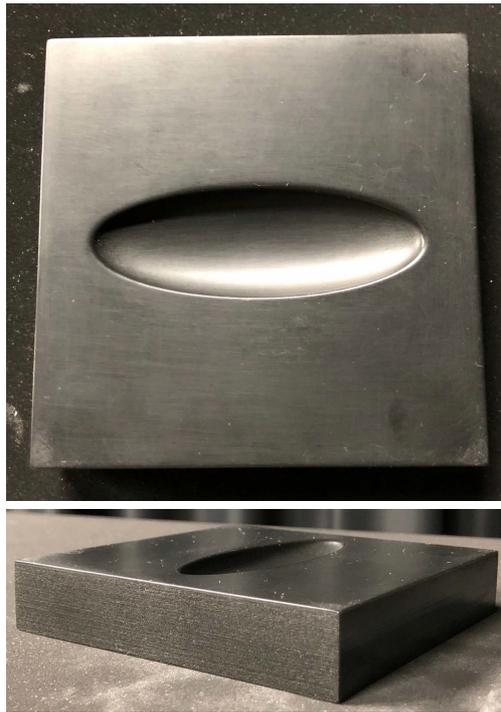


Fig 12 Target object [ellipsoid].

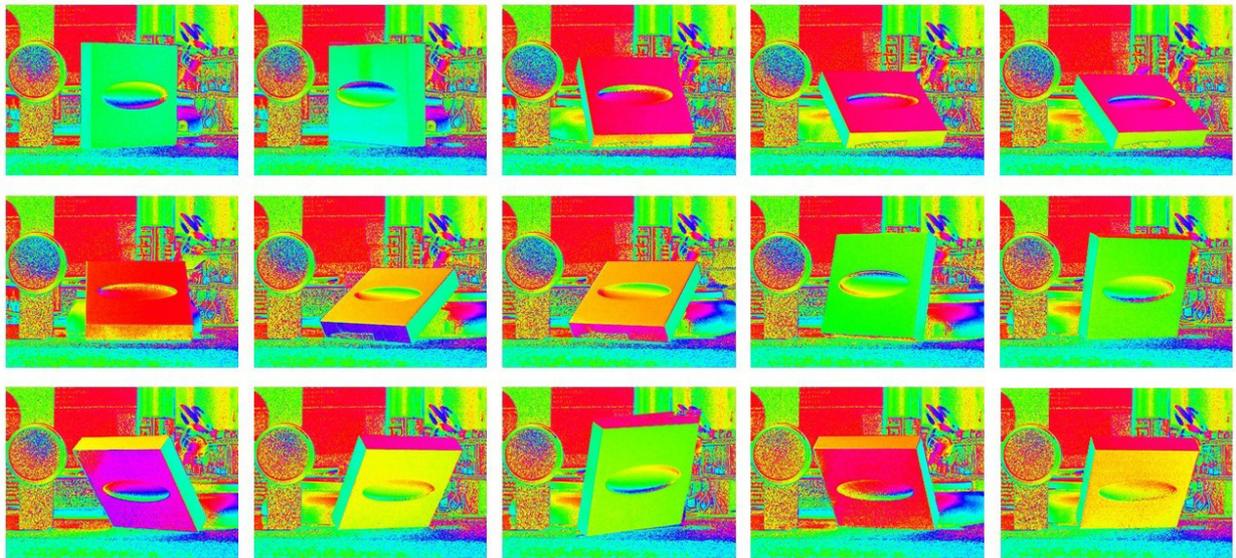


Fig 13 Input image [ellipsoid].

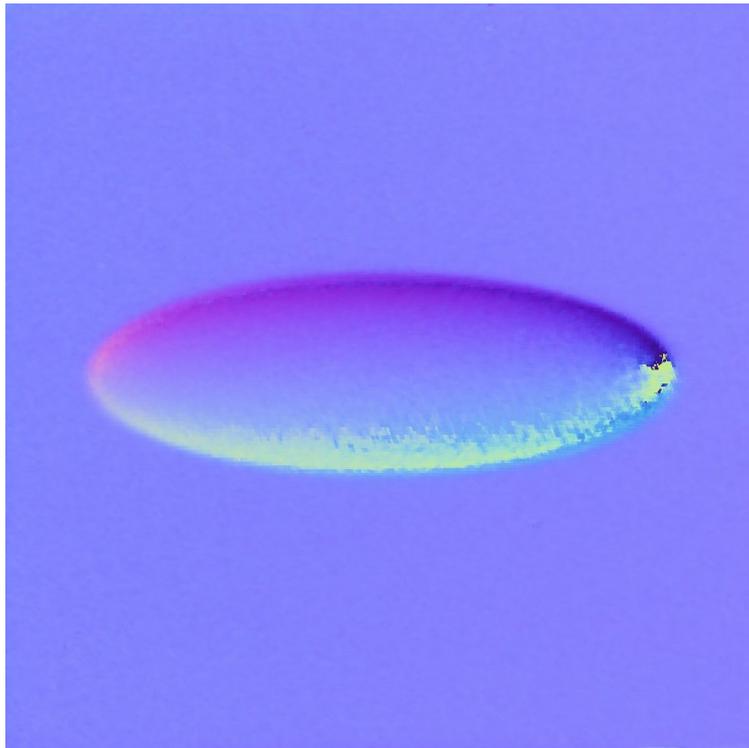


Fig 14 Estimated surface normal [ellipsoid].

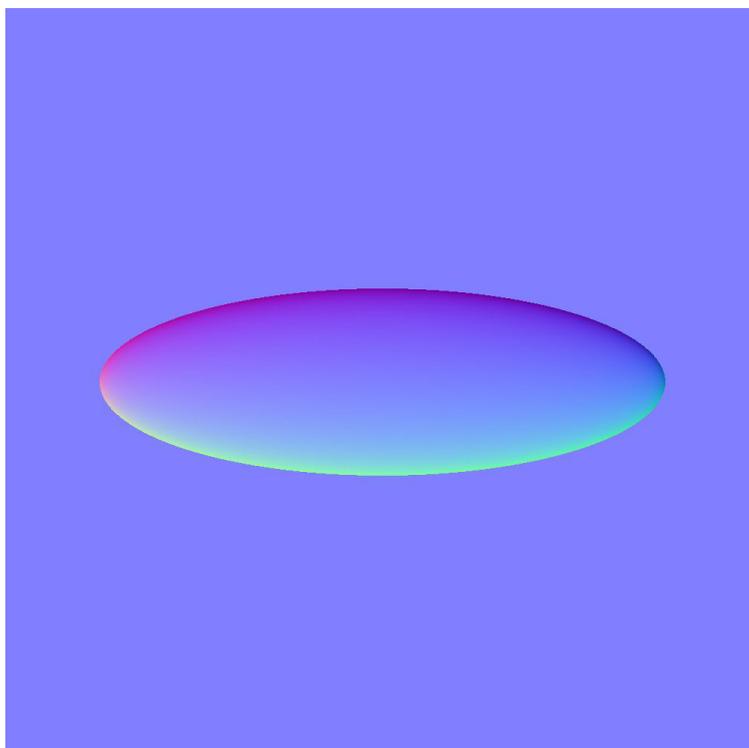


Fig 15 Ground truth of surface normal [ellipsoid].

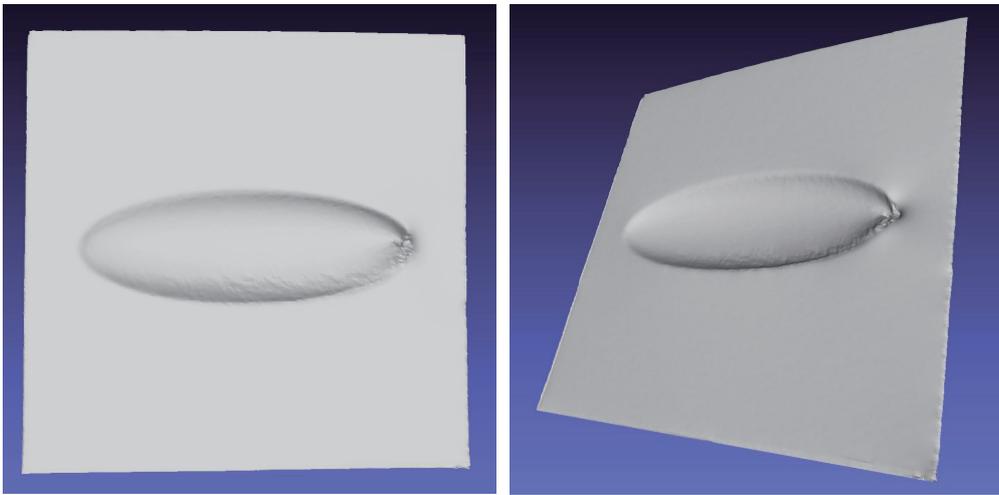


Fig 16 Estimated shape [ellipsoid].

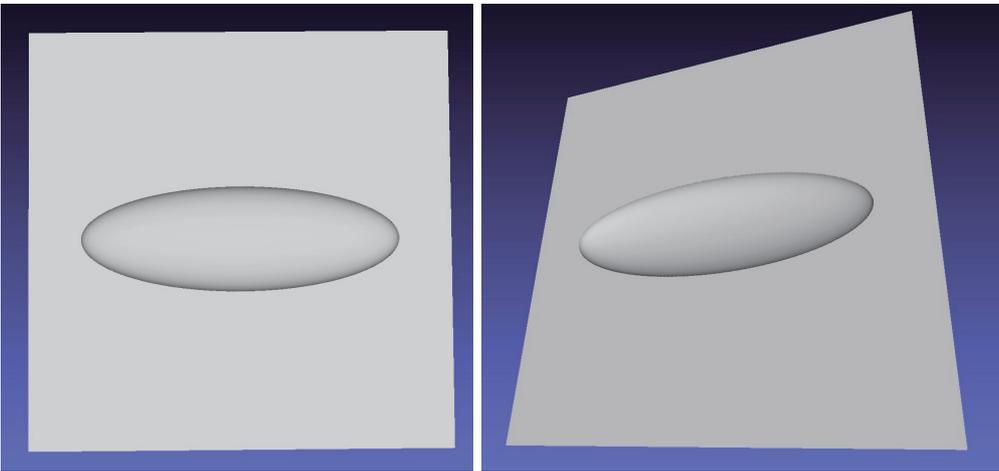


Fig 17 Ground truth of shape [ellipsoid].

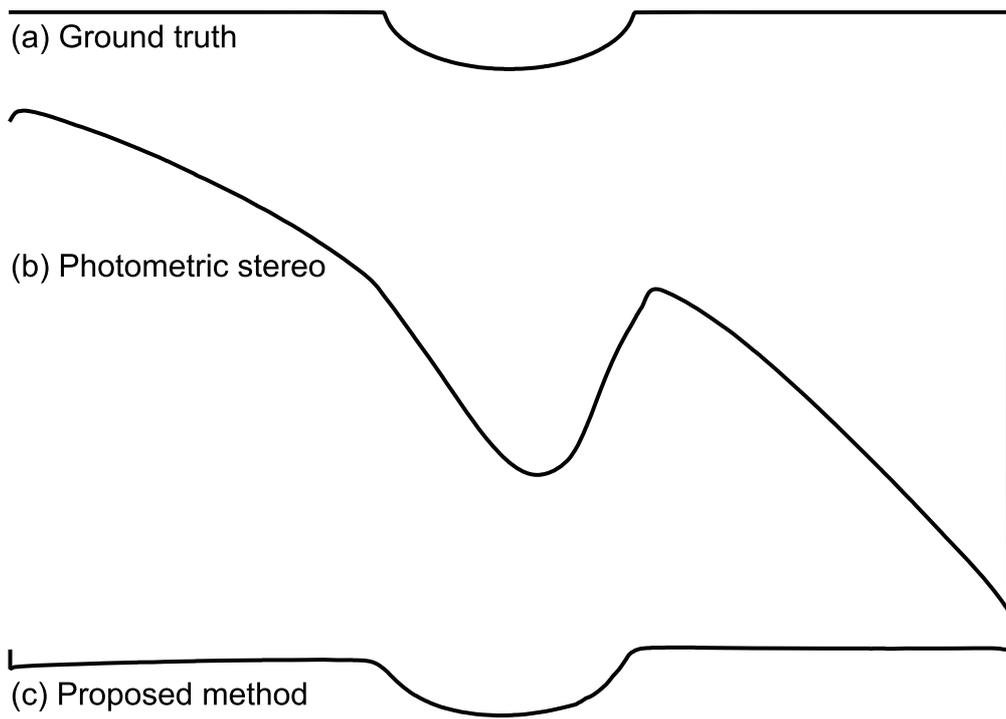


Fig 18 Intersection shape [ellipsoid]: (a) Ground truth, (b) photometric stereo, and (c) proposed method.

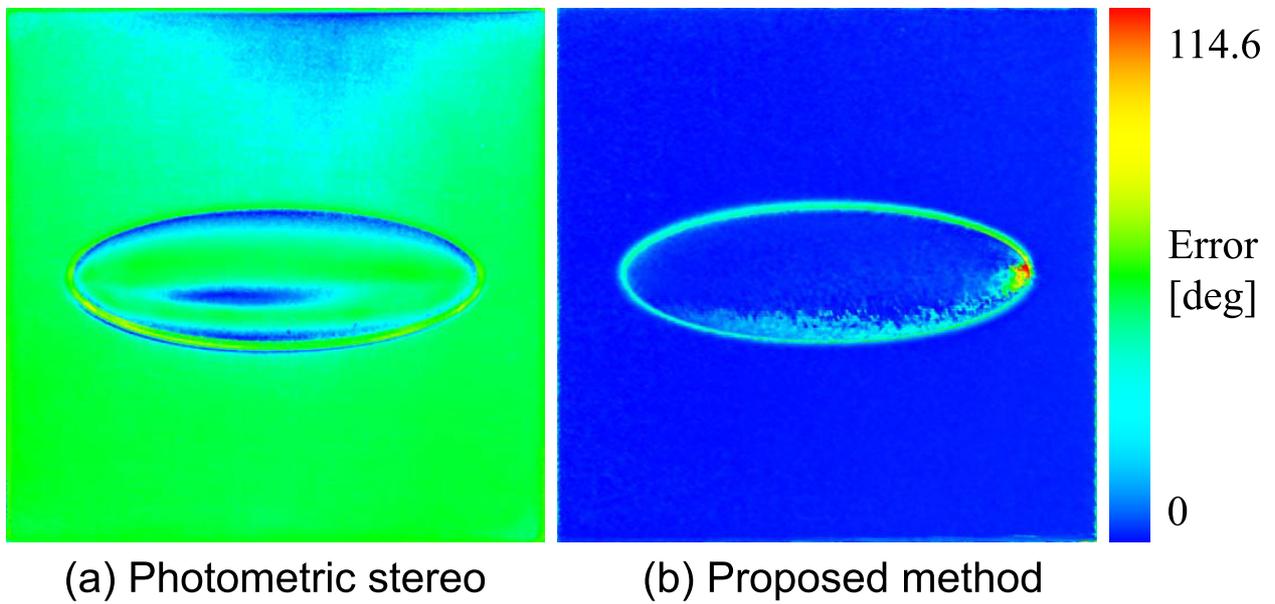


Fig 19 Estimation error [ellipsoid]: (a) Photometric stereo and (b) proposed method.

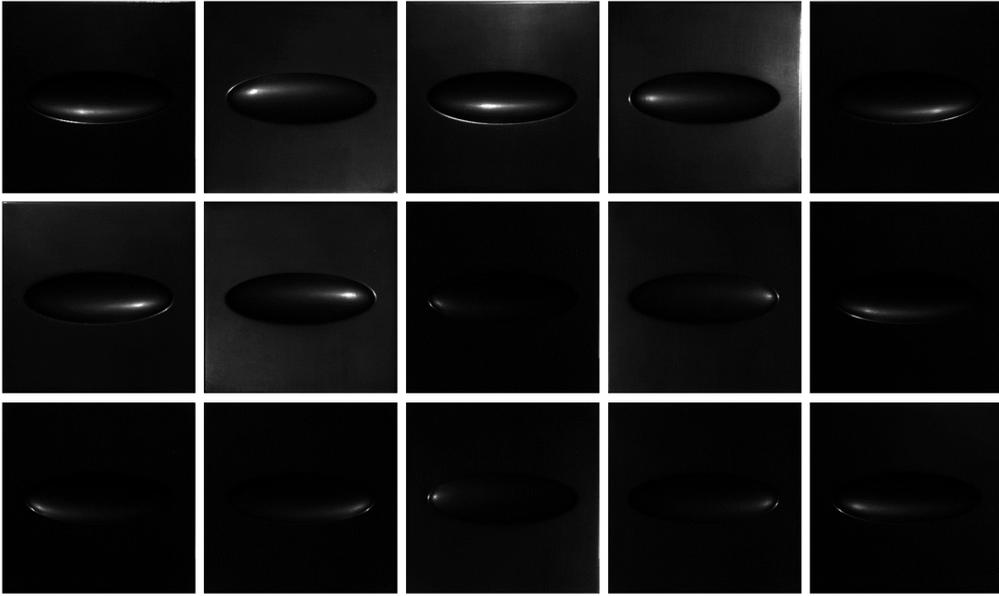


Fig 20 Input image of photometric stereo [ellipsoid].

231 is shown in Fig. 19 (a), and the average error was 42.3 [deg]. Since our error is 4.49 [deg], the
 232 performance of our method is better.

233 3.5 Result of convex object

234 Our method can not only be applied to concave objects but also be applied to convex objects.
 235 In order to prove the wide applicability of our method, we measure a convex object. The target
 236 object is shown in Fig. 23. The input images of our method is shown in Fig. 24, while those of
 237 photometric stereo is shown in Fig. 25. The surface normal of the ground truth, the photometric
 238 stereo, and the proposed method is shown in Fig. 26, Fig. 27, and Fig. 28. The shape of the ground
 239 truth, the photometric stereo, and the proposed method is shown in Fig. 29, Fig. 30, and Fig. 31.
 240 The cross section of the shape of the ground truth, the photometric stereo, and the proposed method
 241 is shown in Fig. 32 (a), Fig. 32 (b), and Fig. 32 (c). The error of the photometric stereo and the
 242 proposed method is shown in Fig. 33 (a) and Fig. 33 (b). The average error of the photometric
 243 stereo was 47.0 [deg] while that of the proposed method was 12.9 [deg].

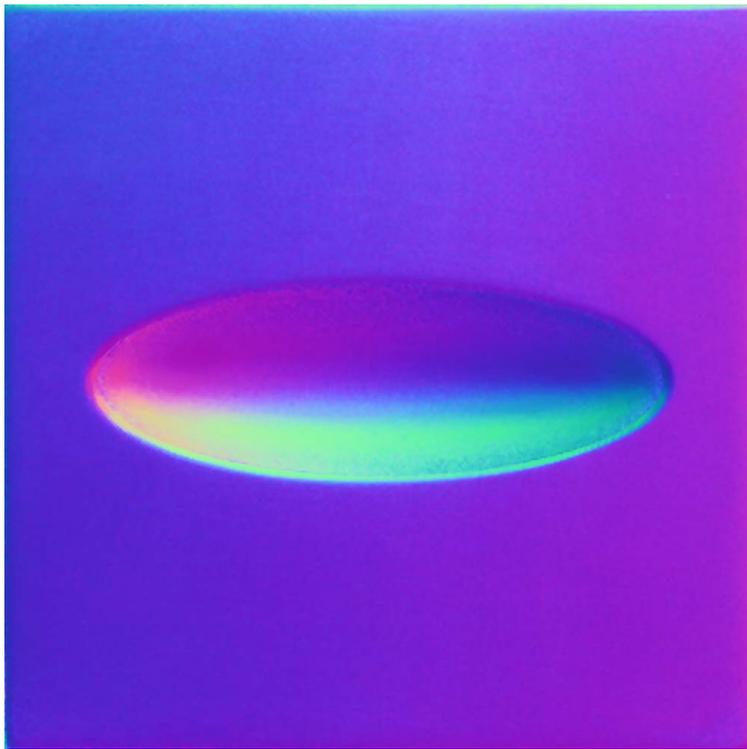


Fig 21 Surface normal of photometric stereo [ellipsoid].

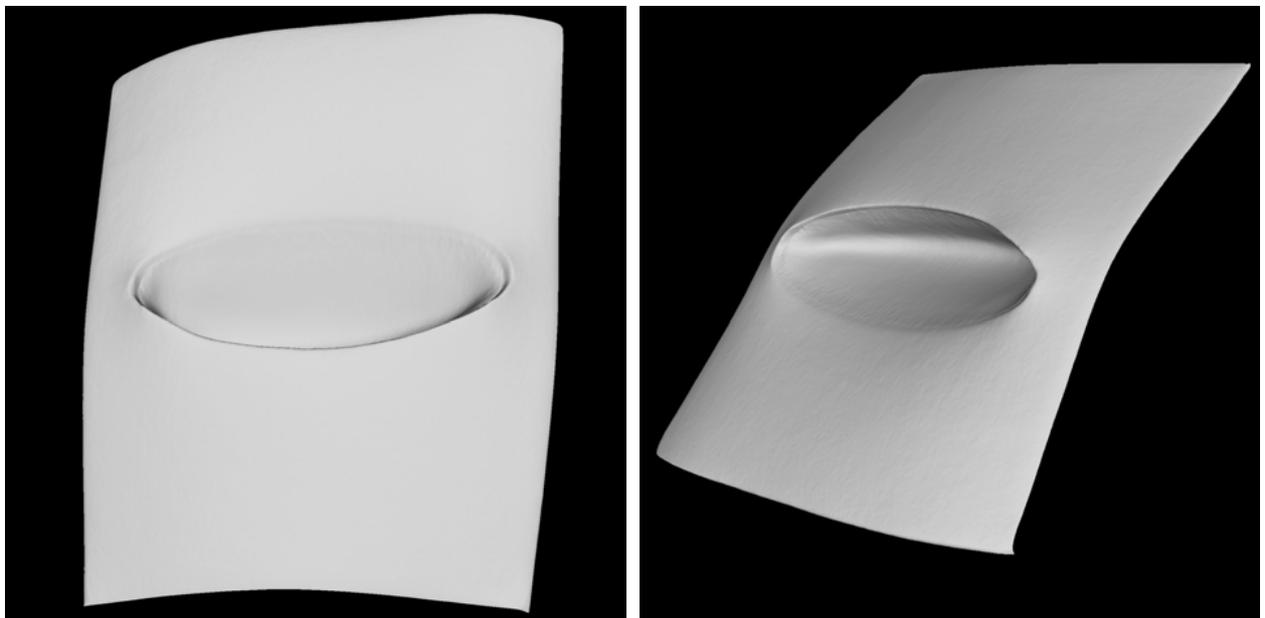


Fig 22 Shape of photometric stereo [ellipsoid].



Fig 23 Photograph of target object [convex].



Fig 24 Input data of our method [convex].

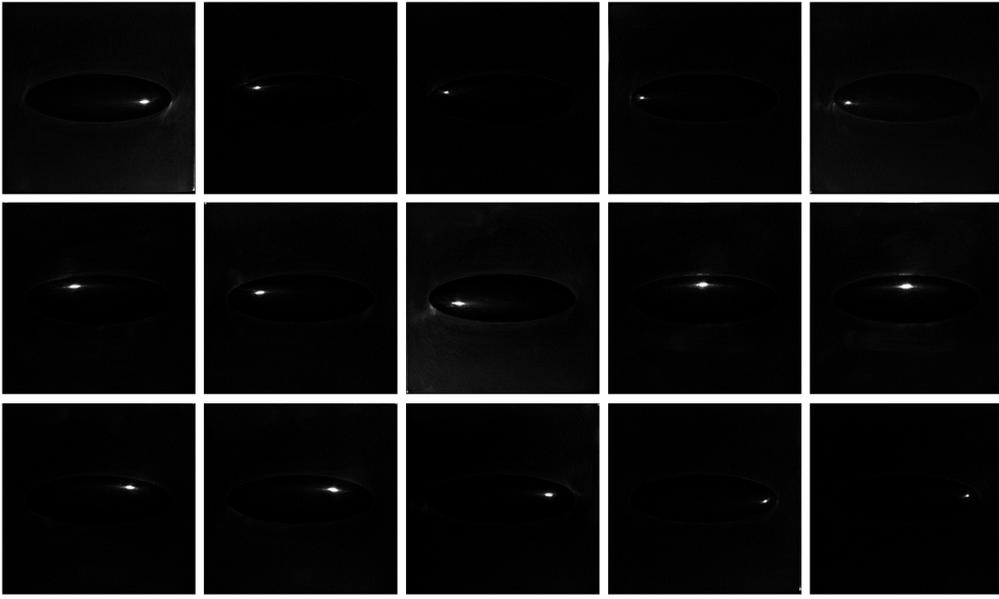


Fig 25 Input images of photometric stereo [convex].

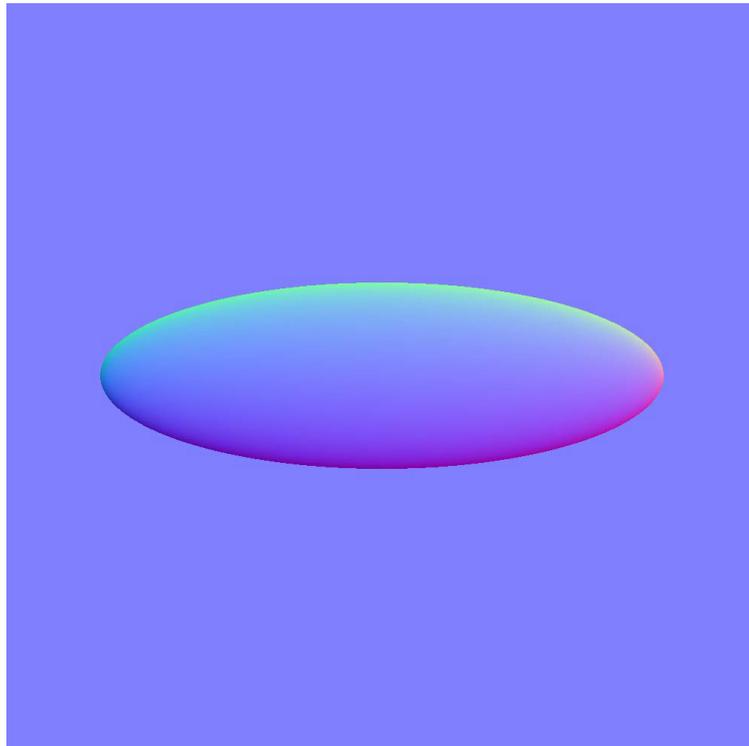


Fig 26 Surface normal of ground truth [convex].

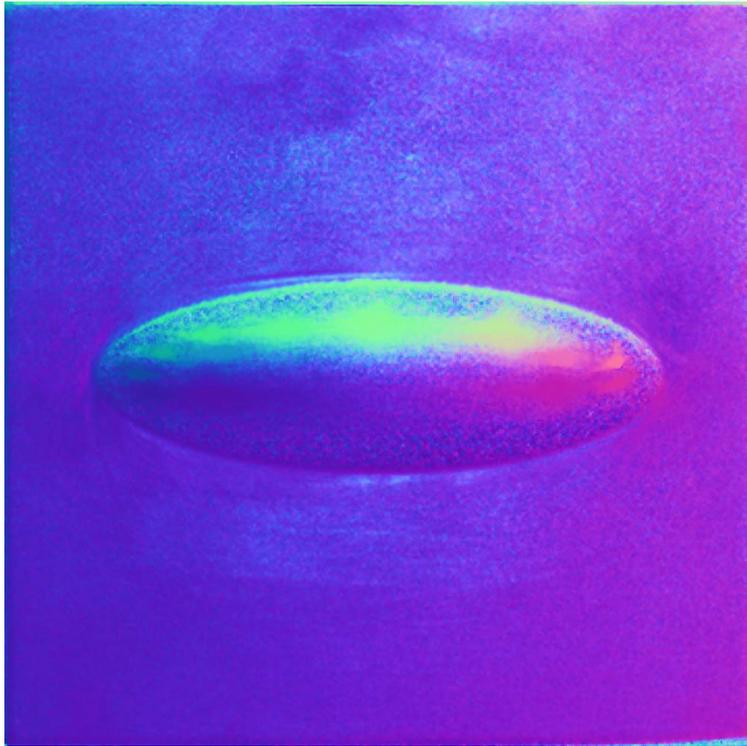


Fig 27 Surface normal of photometric stereo [convex].

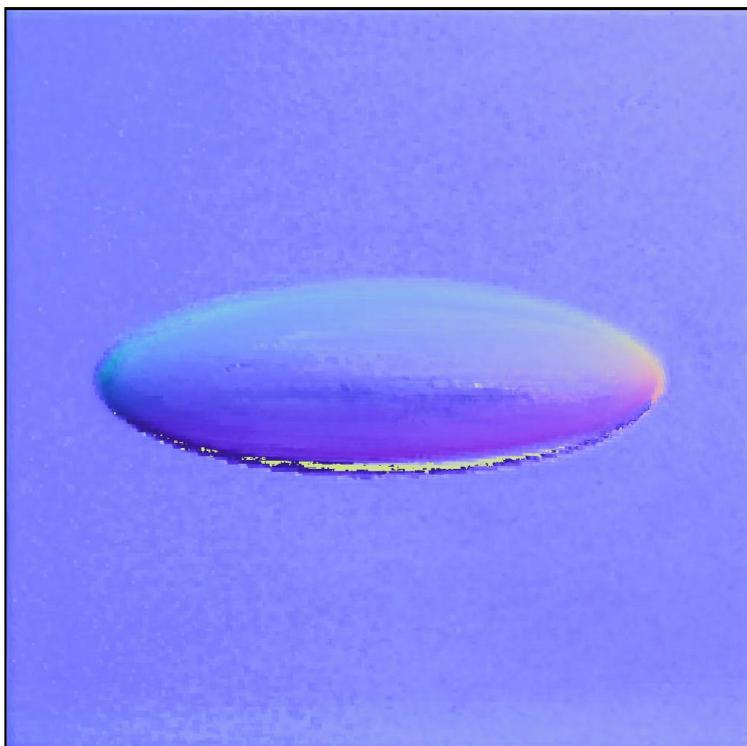


Fig 28 Surface normal of proposed method [convex].

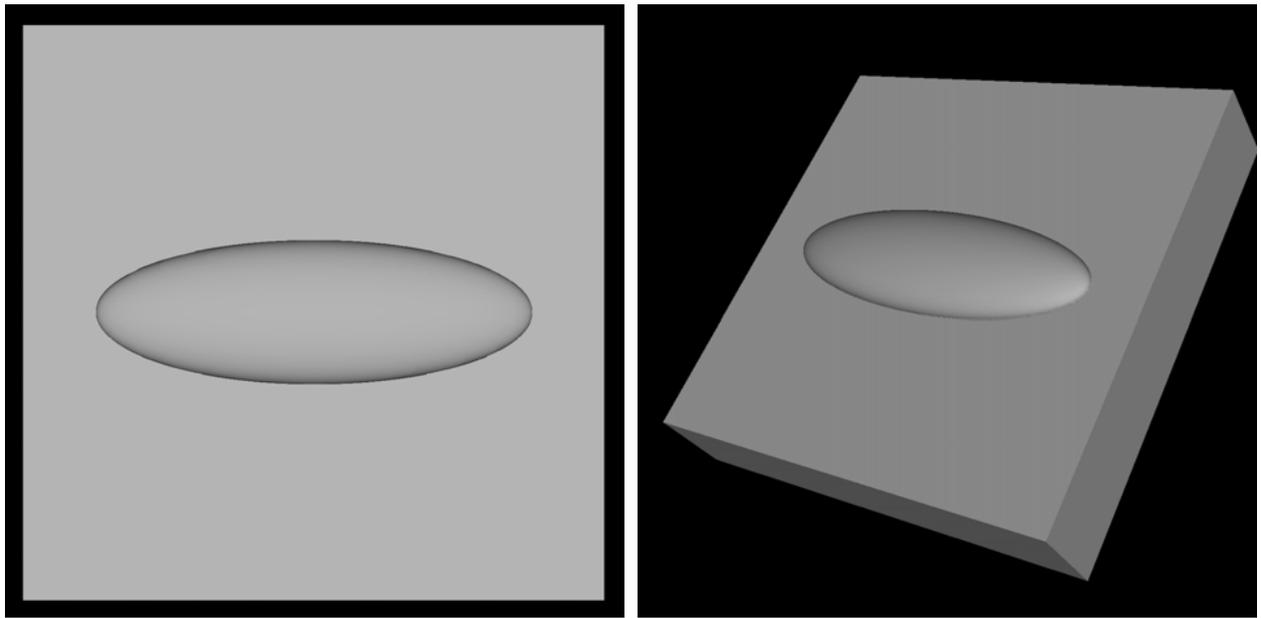


Fig 29 Shape of ground truth [convex].

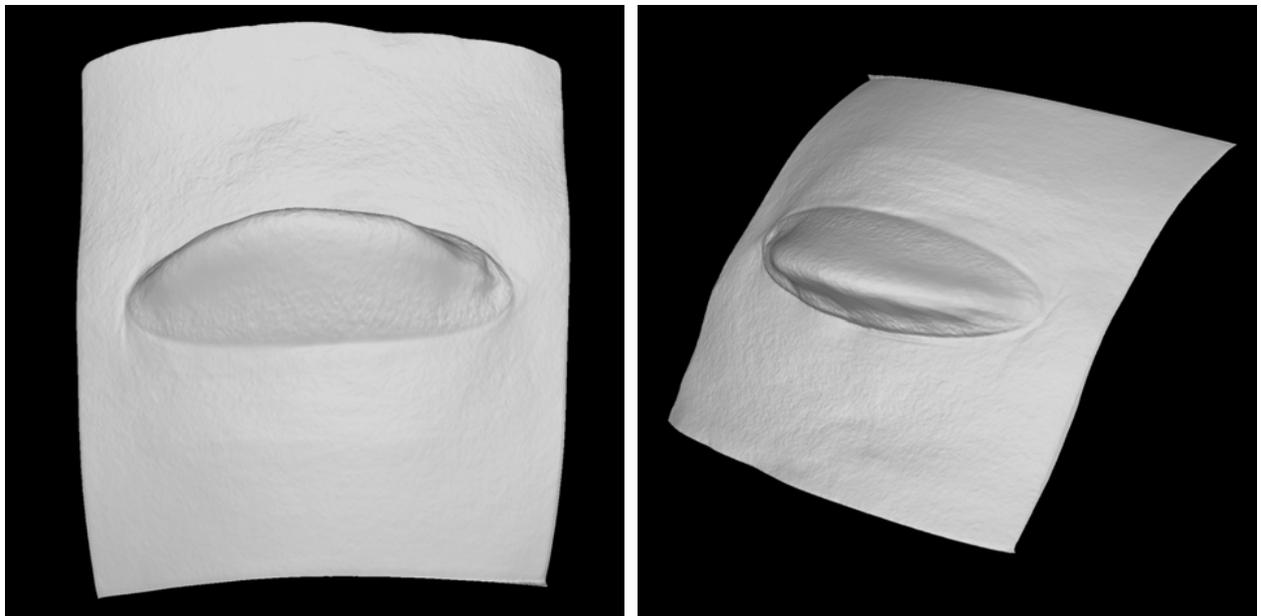


Fig 30 Shape of photometric stereo [convex].

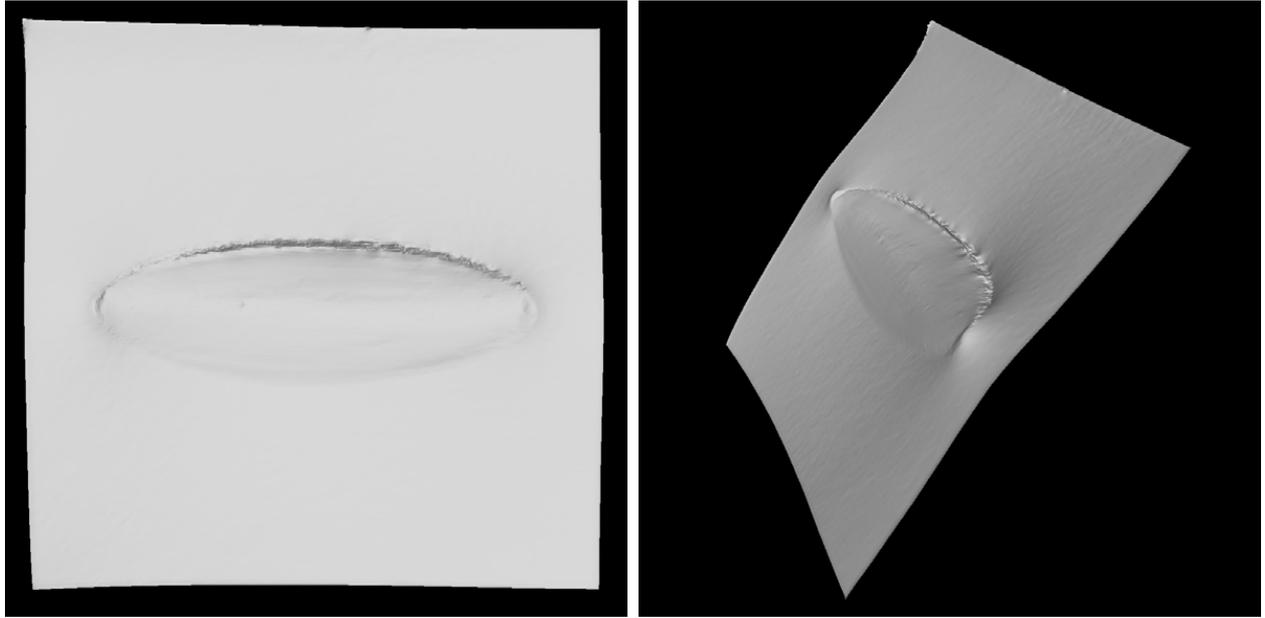


Fig 31 Shape of proposed method [convex].

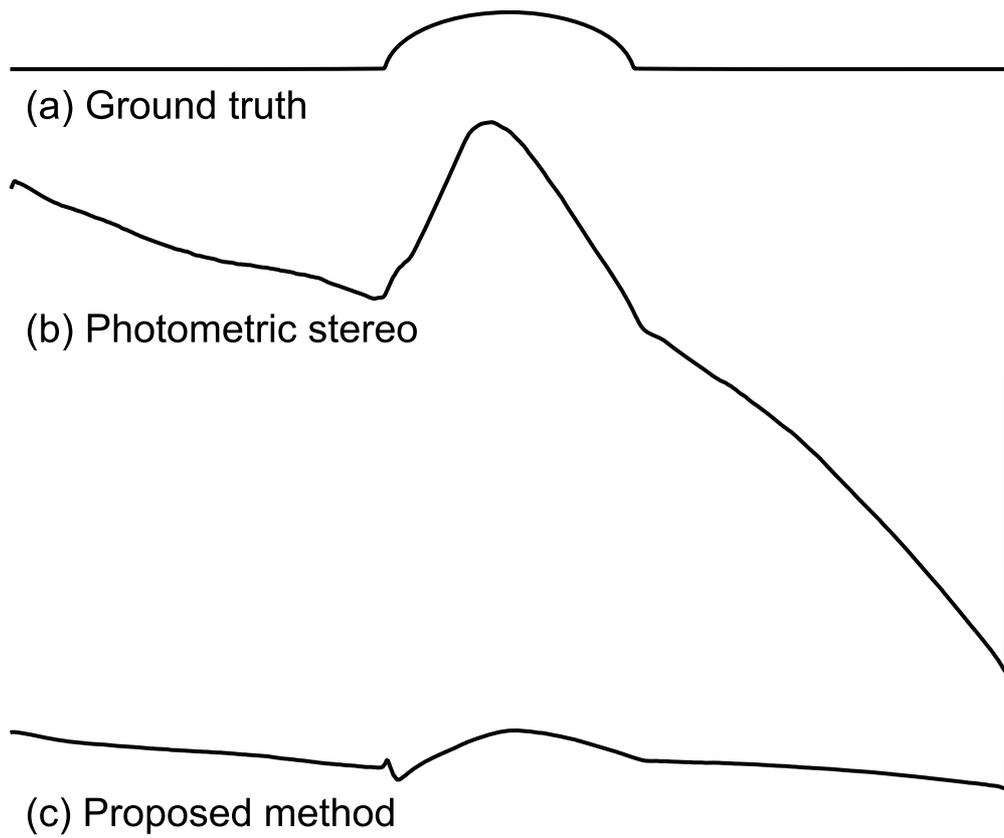


Fig 32 Intersection shape [convex]: (a) Ground truth, (b) photometric stereo, and (c) proposed method.

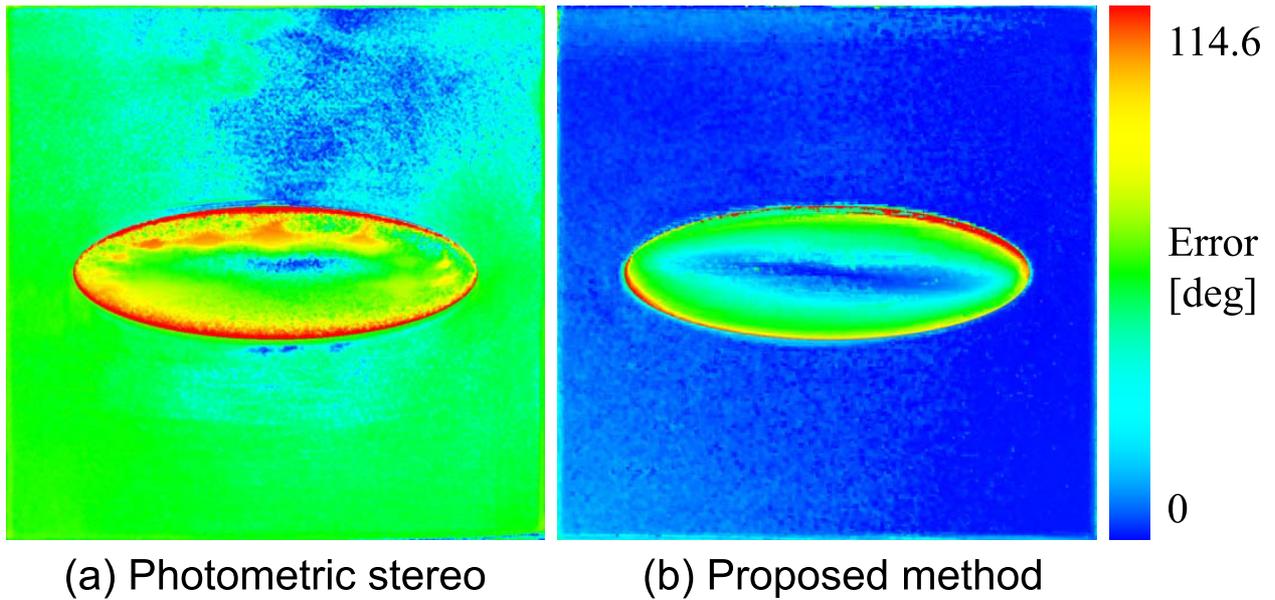


Fig 33 Estimation error [convex]: (a) Photometric stereo and (b) proposed method.

244 *3.6 Result of stripes*

245 In order to evaluate the performance of our method depending on the width of cracks, three differ-
 246 ent concave shapes with different width are measured. Fig. 34 shows the target object and Fig. 35
 247 shows the input images. Also, 15 images are taken, one for each direction. Surface normal of our
 248 method is shown in Fig. 36, and that of ground truth is shown in Fig. 37. The estimated shape is
 249 shown in Fig. 38 and Fig. 40 (b), while ground truth is shown in Fig. 39 and Fig. 40 (a). The error
 250 map is shown in Fig. 41, and the average error was 7.18 [deg].

251 *3.7 Result of worm*

252 In order to simulate an acutal situation, we applied our method to a cracks which is not shaped in
 253 a straight line. Fig. 42 shows the target object, Fig. 43 shows the input images, Fig. 44 shows the
 254 estimated surface normal, and Fig. 45 shows the estimated shape.



Fig 34 Target object [stripe].

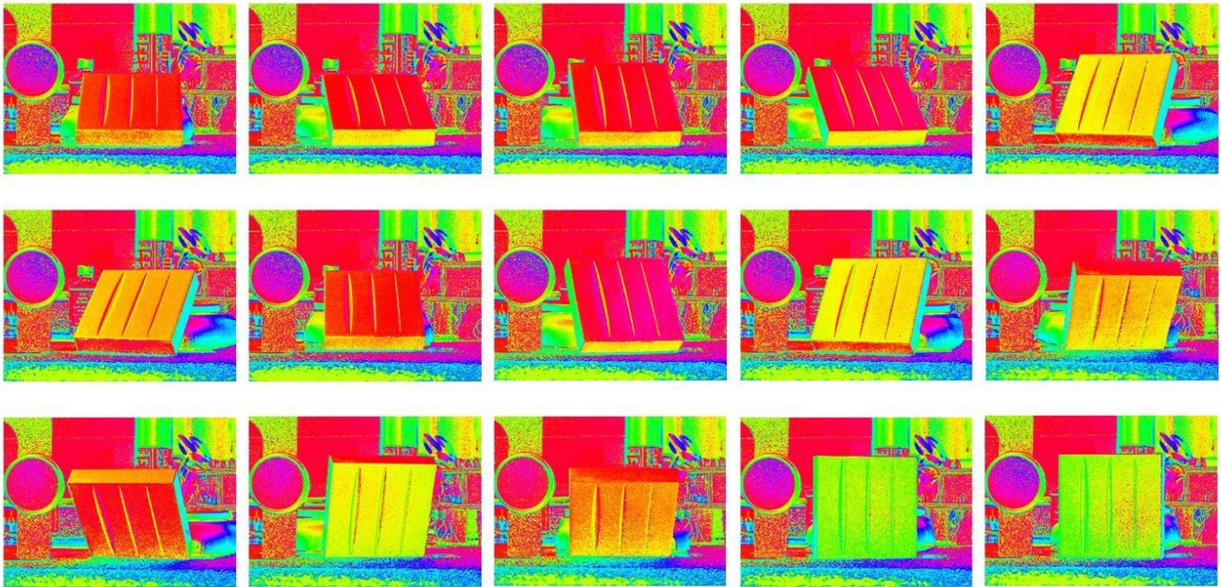


Fig 35 Input images [stripe].

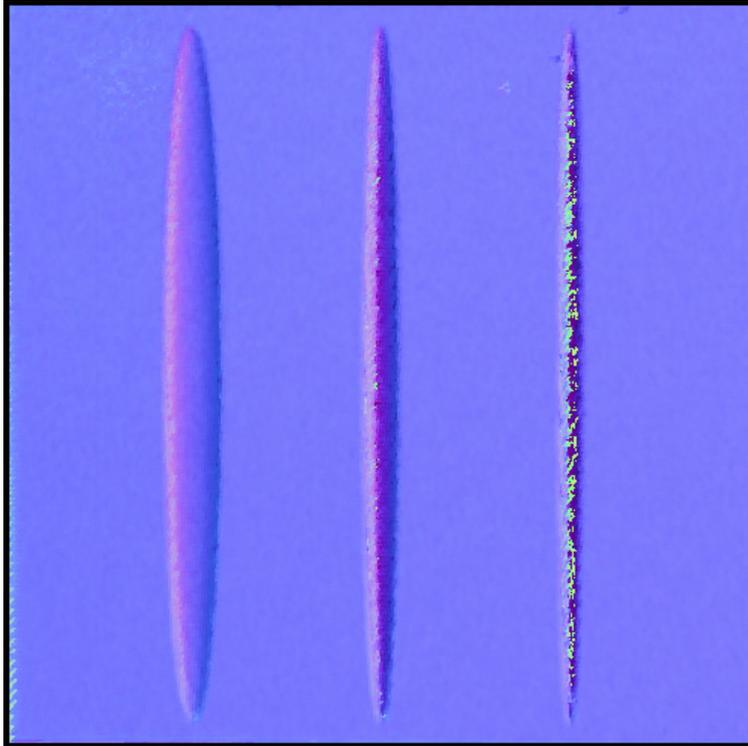


Fig 36 Estimated surface normal [stripe].

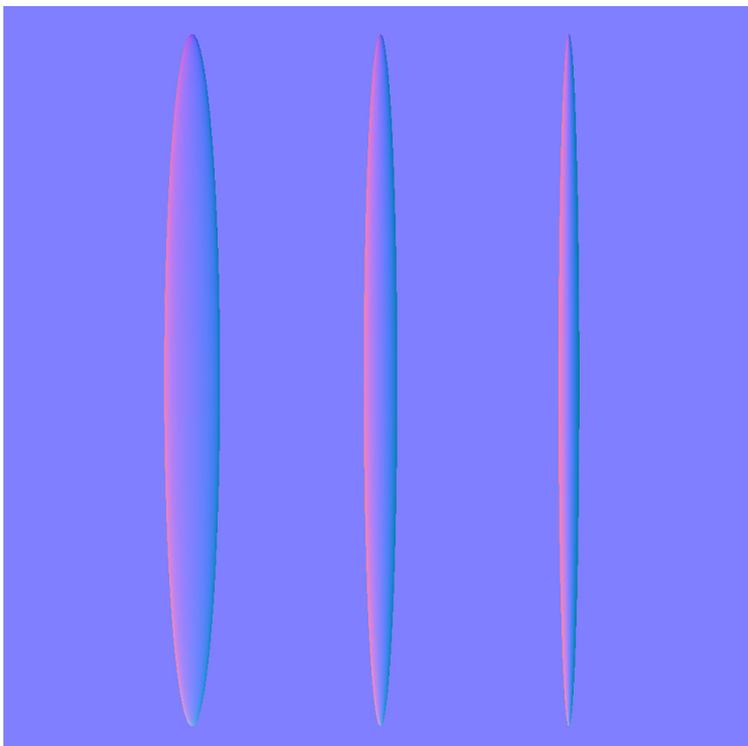


Fig 37 Ground truth of surface normal [stripe].

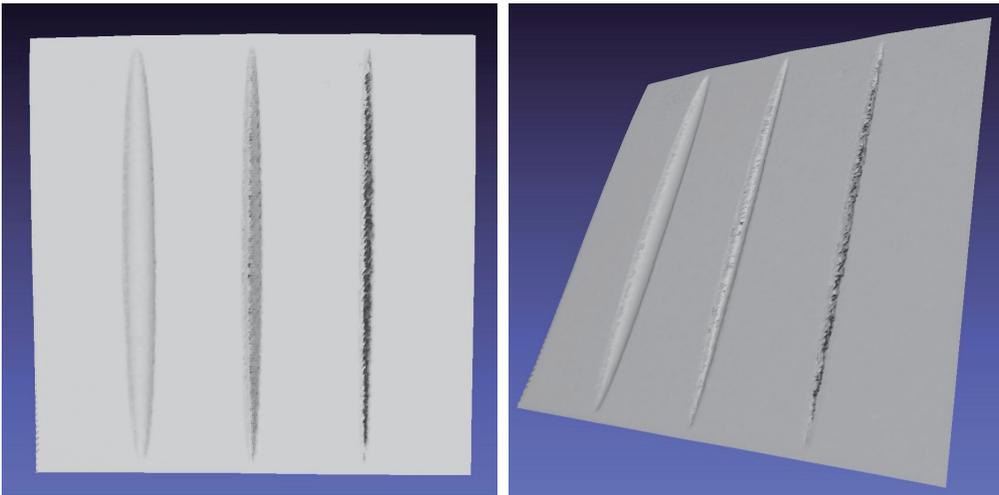


Fig 38 Estimated shape [stripe].

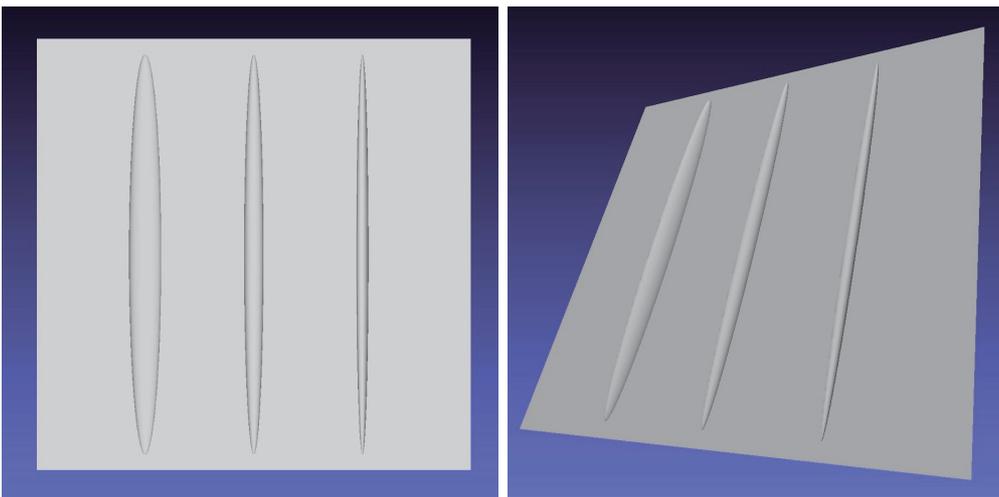


Fig 39 Ground truth of shape [stripe].

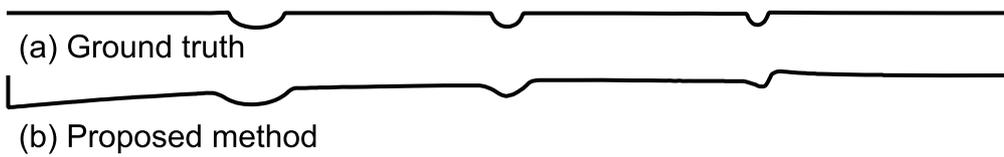


Fig 40 Intersection shape [stripe]: (a) Ground truth and (b) estimated shape.

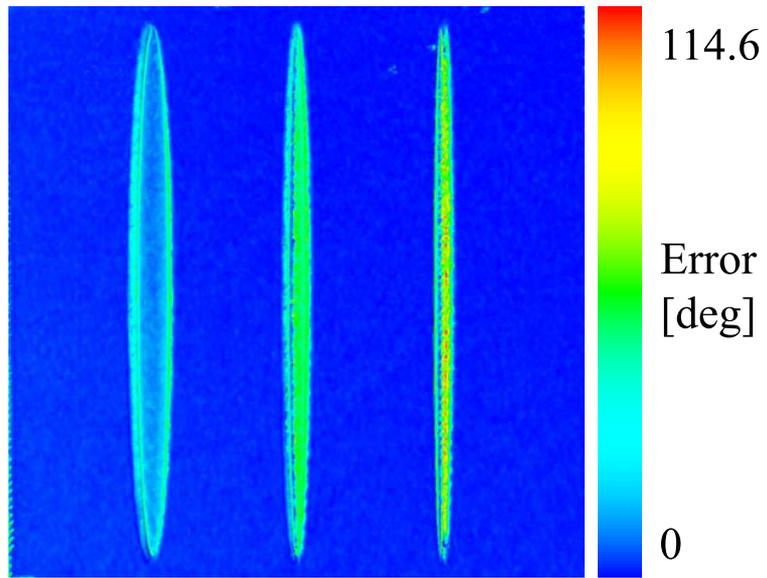


Fig 41 Error of our method [stripe].



Fig 42 Target object [worm].

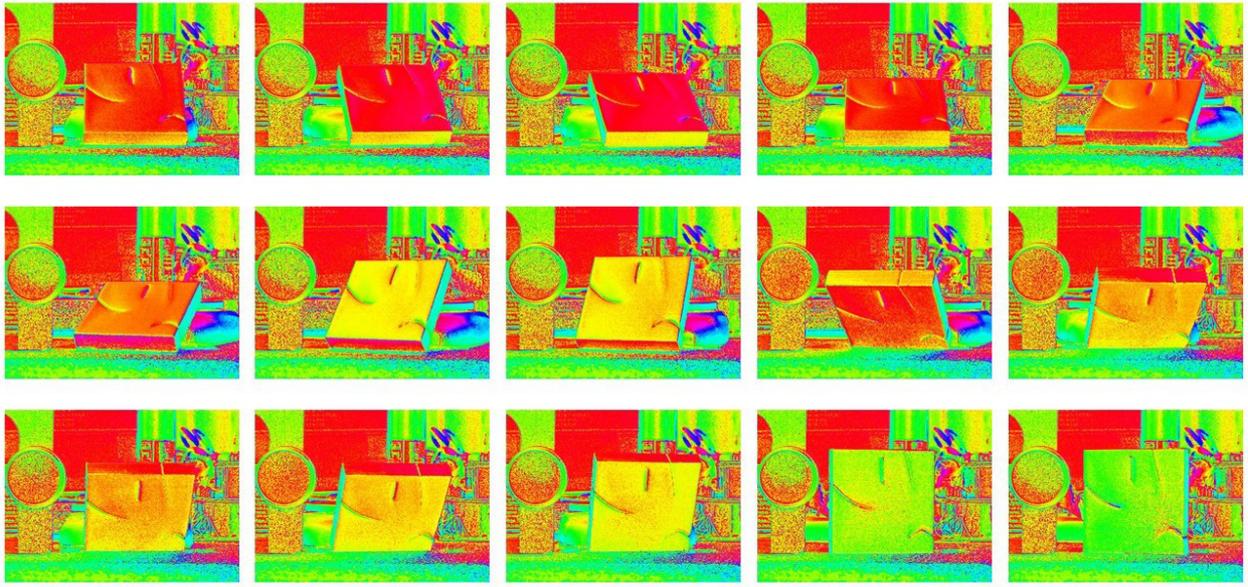


Fig 43 Input images [worm].

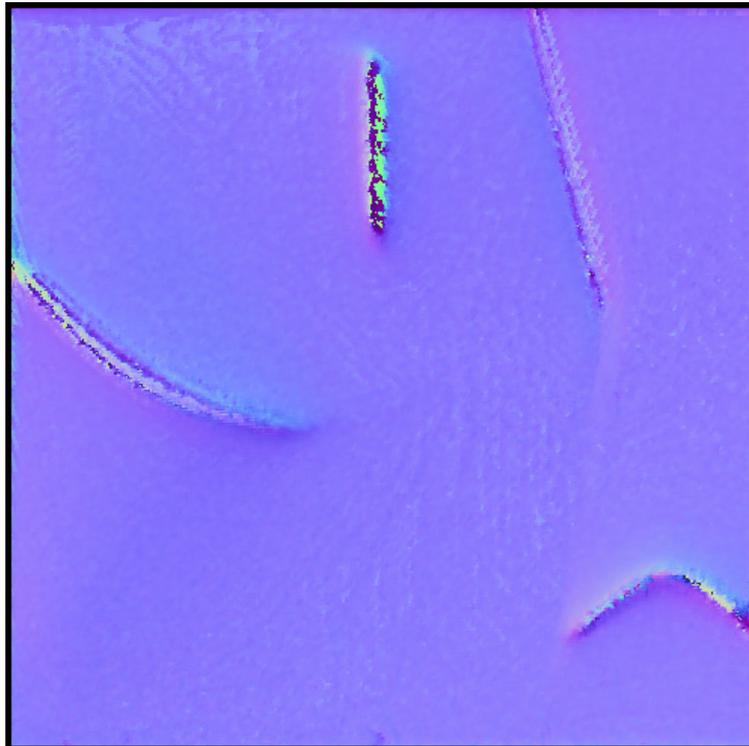


Fig 44 Estimated surface normal [worm].

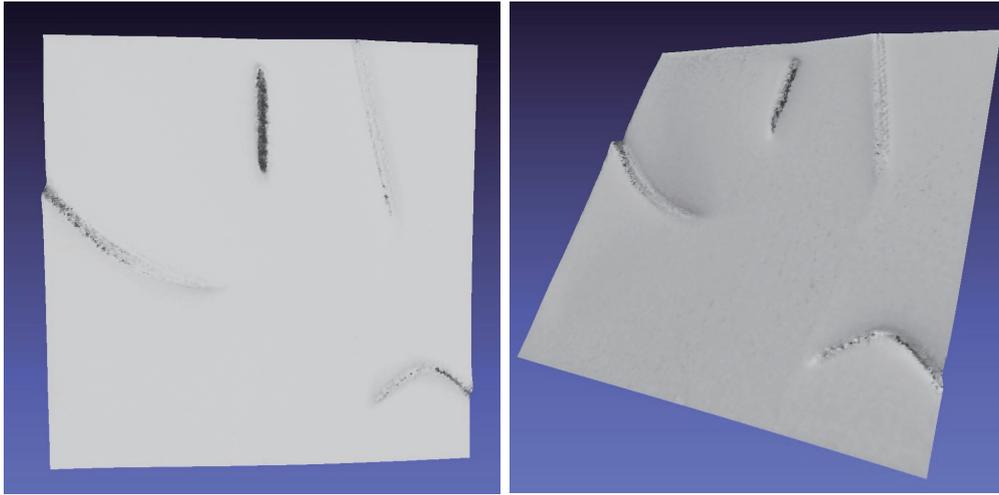


Fig 45 Estimated shape [worm].

255 3.8 Discussion

256 As is shown in Fig. 41, the narrower the concave part is, the worse the result is. This is because
257 the light is not illuminated satisfactorily to the narrow concave part. In addition, interreflection
258 becomes strong at narrow concave part.

259 4 Conclusion

260 We propose a shape estimation method from polarization images obtained from multiple view-
261 points. The proposed method computes the surface normal using SVD to minimize the least-
262 squared error. It can estimate the shapes of concave part of planar objects which is black and has
263 high specularity. It is usually difficult to estimate the shape of planar object with small details,
264 however, our algorithm fully utilizes the property that the target object is almost planar. What
265 is interesting in our method is that even if we assume that the object is planar, the shape of the
266 concave part is also successfully determined.

267 The experiments show that our method can estimate the shape of the crack. This property
268 demonstrates that our method is useful for investigation of product inspection in factory, damage

269 inspection in architecture, age estimation from skin wrinkle, and so on. For example, factories want
270 to know the reason of the defect of the product since they want to fix the problem and decrease the
271 defects. In order to analyze the reason, the shape of the defects is necessary, and our method is
272 useful for this purpose.

273 The disadvantage of our method is that the shape where the light has not reached cannot be
274 estimated. However, this disadvantage does not only apply to our method but also apply to any
275 methods in image processing field since “image” cannot be observed if the scene is not illuminated.
276 Our future work is to develop a measurement system which illuminates the target object from any
277 directions.

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